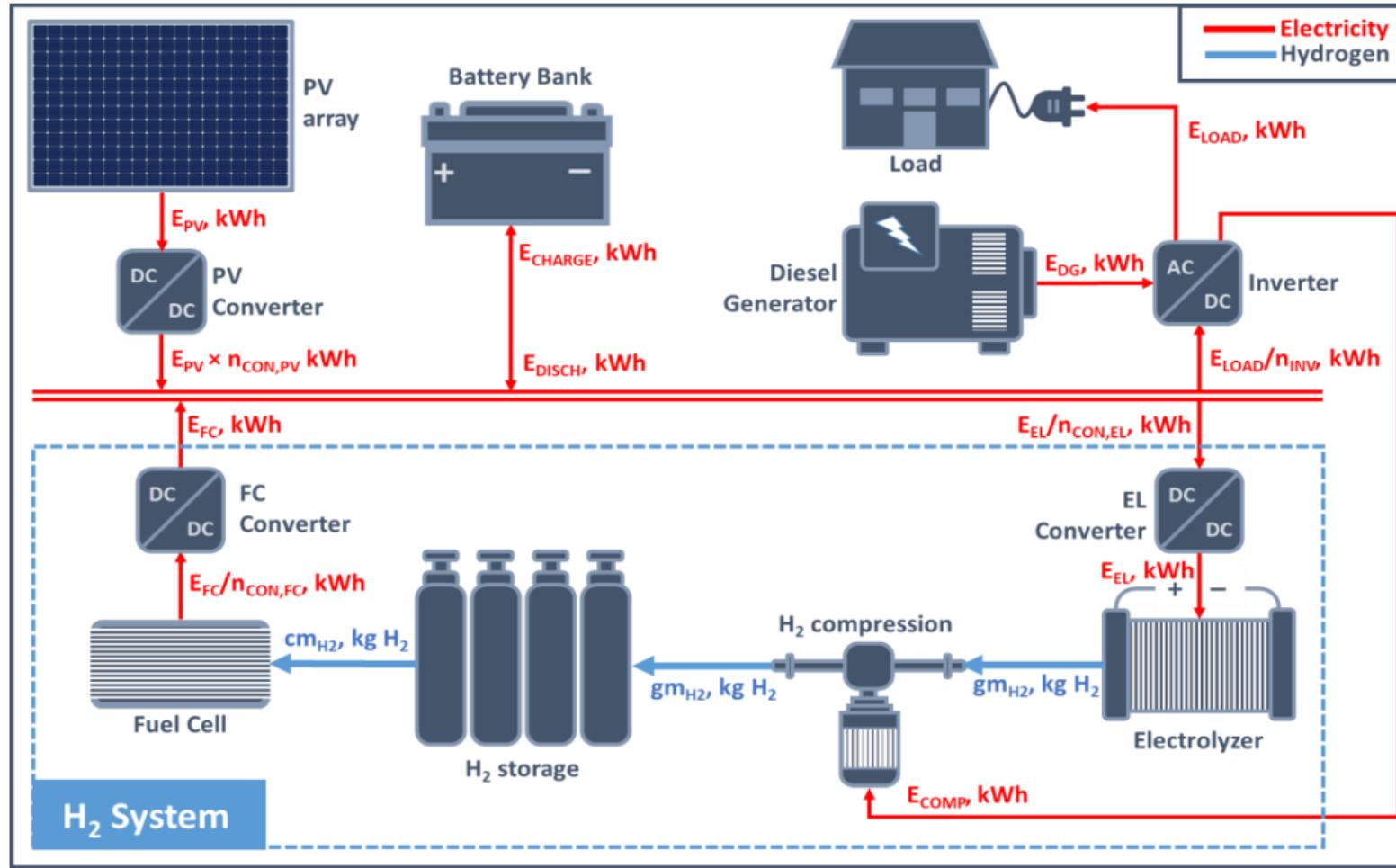
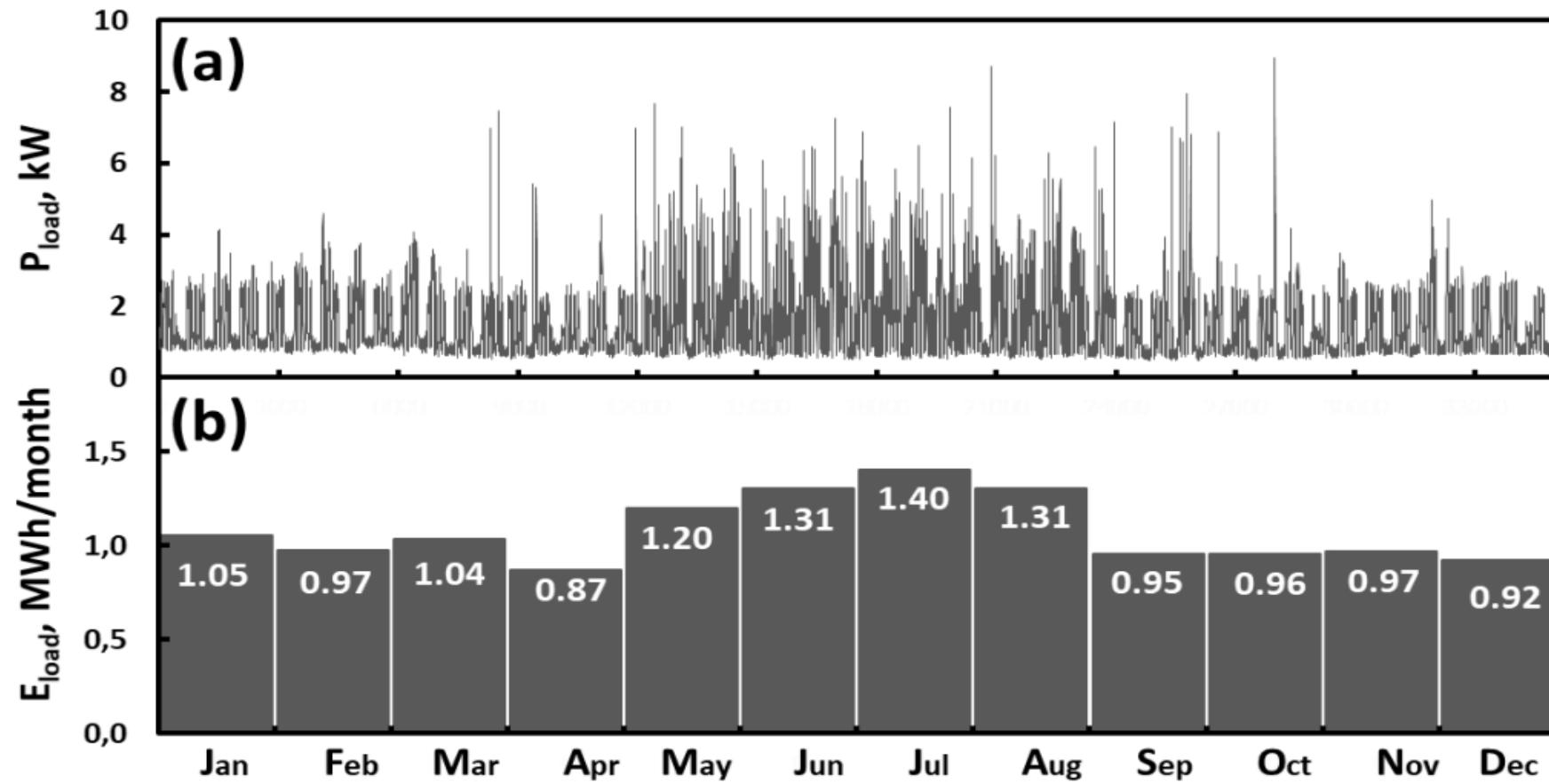


*Power Management Strategy for the effective sizing of
a PV Hybrid Renewable Energy System with
battery and H₂ storage.*

Block diagram of the PV Hybrid Renewable Energy System.

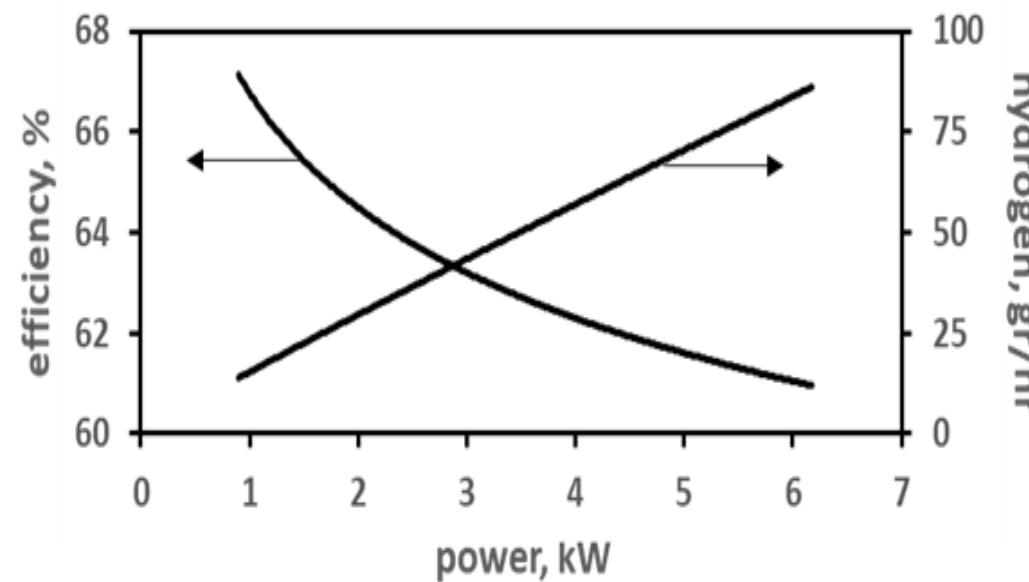


Annual load profile



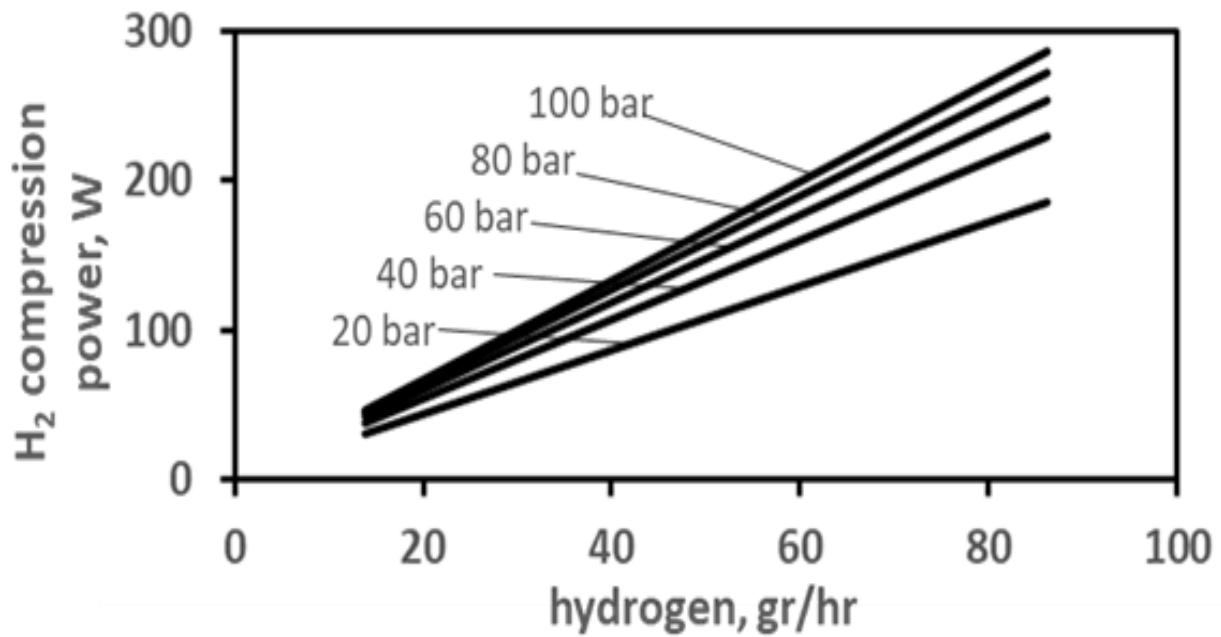
Dependence of the electrolyzer's efficiency and H₂ generation on power consumption.

$$EL_{eff} = 66.8 \times P_{el}^{-0,05}$$



$$GM_{H2} = 0.0153 \times P_{el}^{0.95}$$

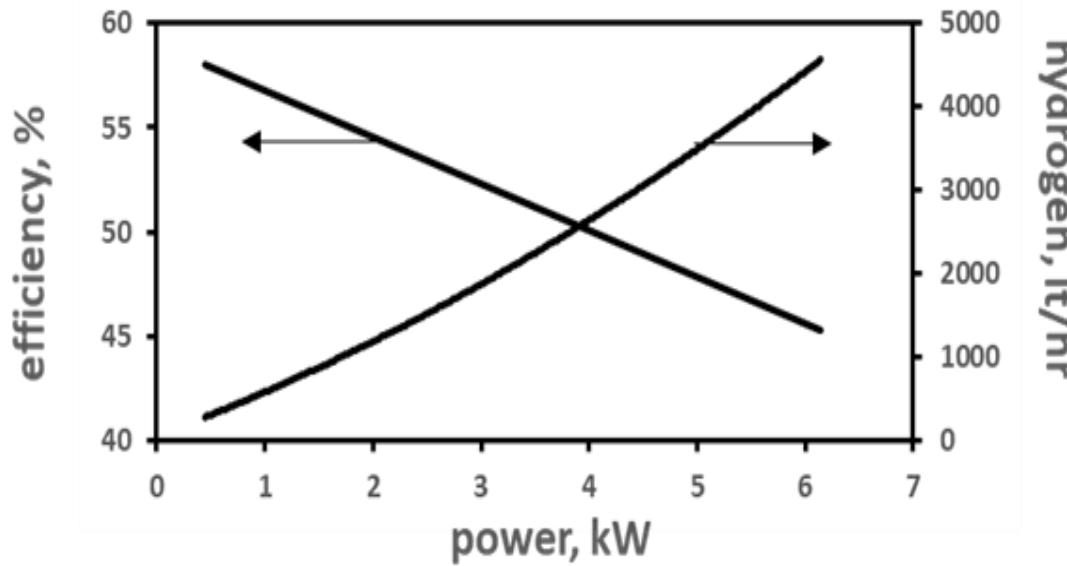
Power consumption for H₂ compression



$$PW_{comp} = (976.62 \times P_{cyl}^{0.27}) \times GM_{H2}$$

Dependence of the fuel cell's efficiency and H₂ consumption on power generation

$$FC_{eff} = 59.0 - 2.23 * P_{FC}$$

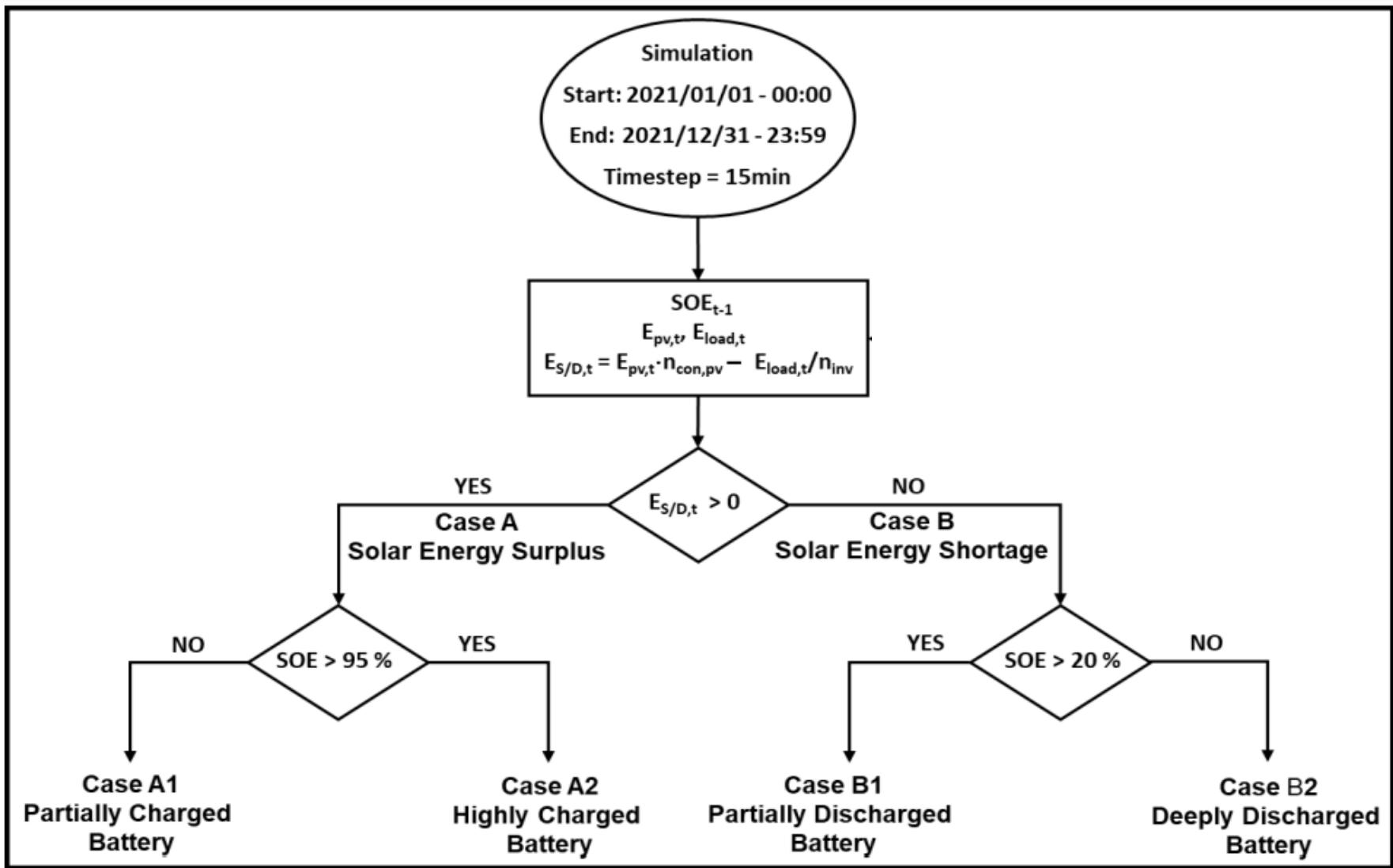


$$CM_{H2} = 2.78 * P_{FC}^2 + 33.17 * P_{FC} + 4.24$$

Design characteristics of the hydrogen system elements

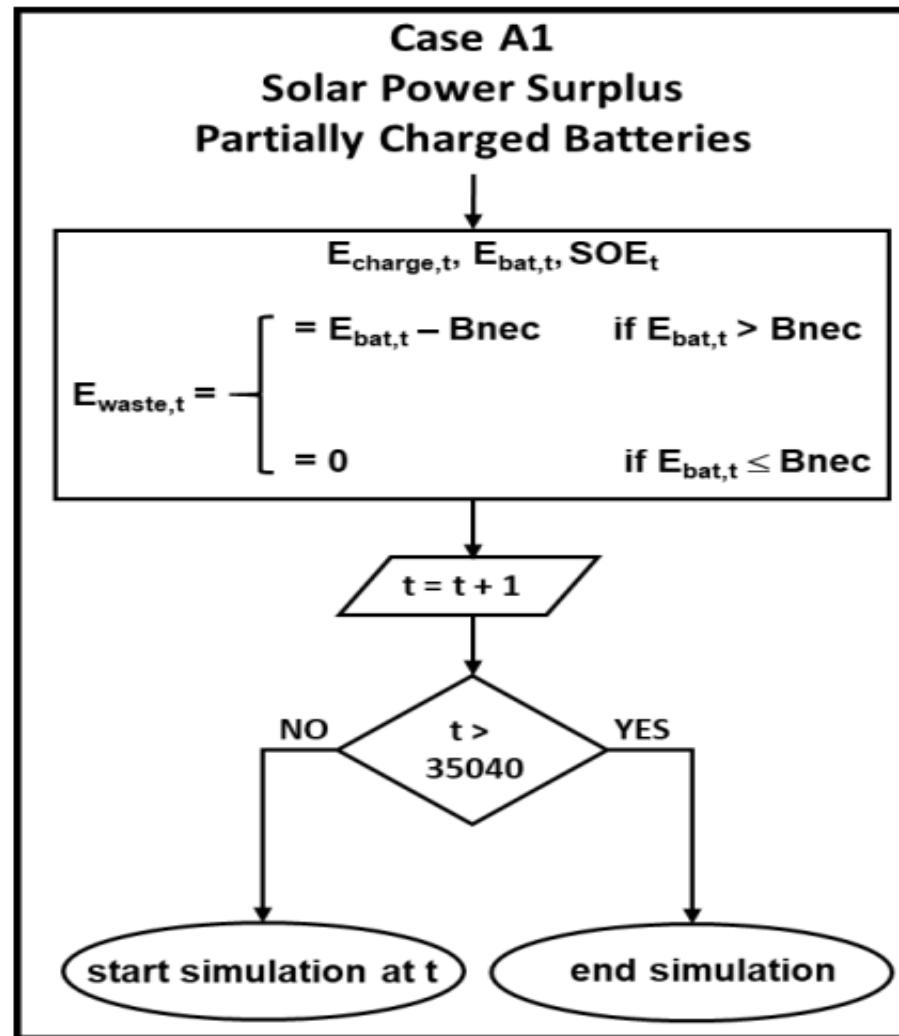
Alkaline Electrolyzer	PEM Fuel Cell		
Power, kW	0.90 – 6.18	Power, kW	0.44 – 6.15
Voltage, V	50 – 56	Voltage, V	67 – 88
Current, A	18 – 111	Current, A	5 – 92
Efficiency, %	60 – 68	Efficiency, %	44 – 59
H ₂ generation, gr/hr	13.9 – 86.2	H ₂ consumption, gr/hr	17.3 – 318.1
Hydrogen Compression	Hydrogen Storage		
Pmax, bar	100	Pmax, bar	100
Power, kW	<0,29	Maximum storage capacity, kgH ₂	30.5 – 53.3
Compression rate, lt(STP)/hr	<1,256	Number of 50 lt cylinders	80 – 140

Flowchart of the Energy Management Strategy



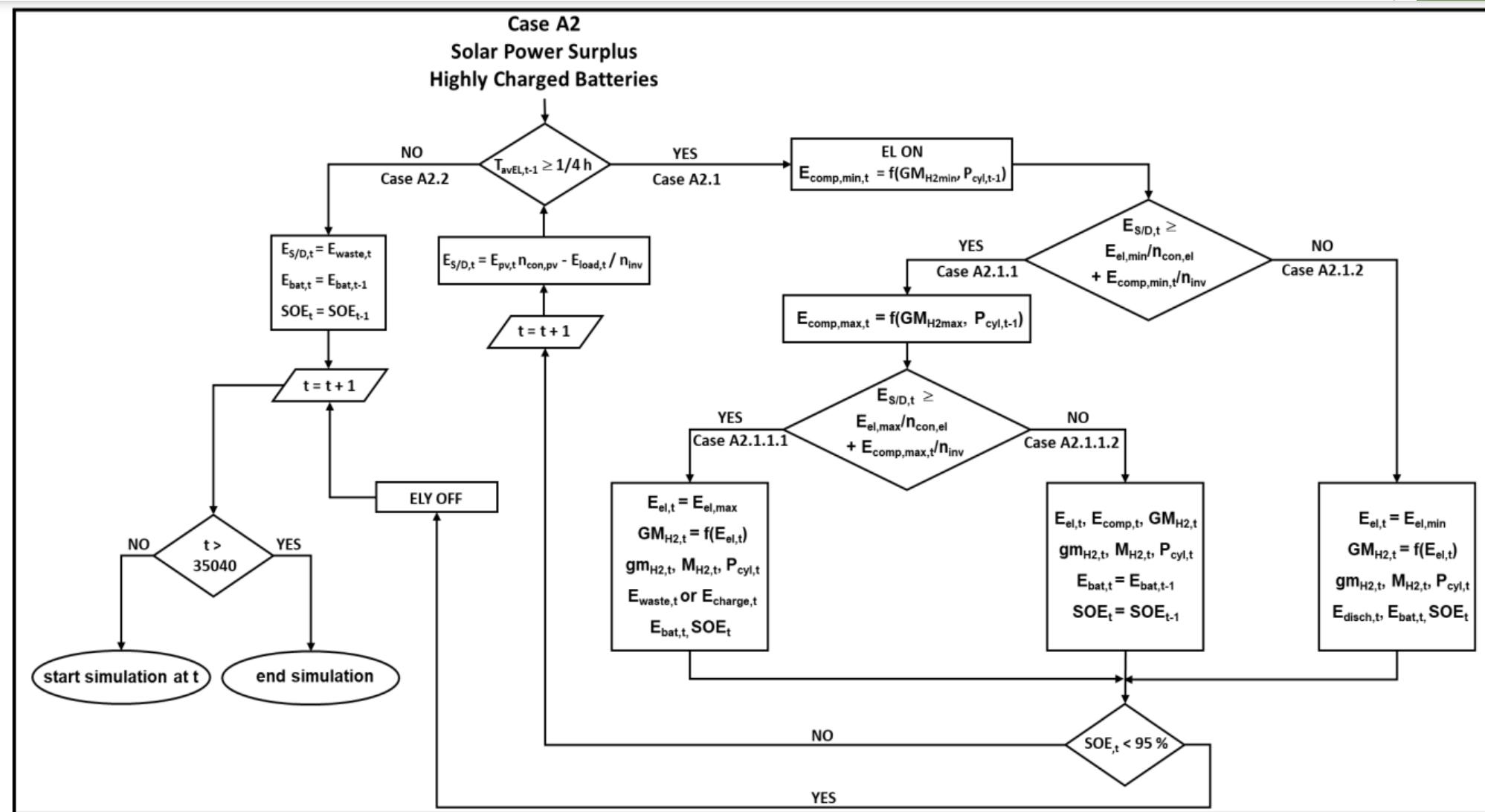
Case A1: Solar Energy Surplus – Partially Charged Battery

$$E_{S/D,t} > 0 \text{ and } SOE < 95\%$$



Case A2: Solar Energy Surplus – Highly Charged Battery

$E_{S/D,t} > 0$ and $SOE > 95\%$



Case A2: Solar Energy Surplus – Highly Charged Battery

H₂ storage availability variable:

$$T_{avEL,t-1} = \frac{M_{H2,max} - M_{H2,t-1}}{GM_{H2,max}}$$

$M_{H2,max}$

is the maximum mass of H₂ that can be stored in kg,

$M_{H2,t-1}$

is the mass of stored hydrogen, at time “t-1”, in kg, and

$GM_{H2,max}$

is the maximum H₂ production rate, in kg/hr. $GM_{H2} = 0.0153 \times P_{el}^{0.95}$

Case A2: Solar Energy Surplus – Highly Charged Battery

Case A2.1.1.1 $E_{S/D,t} \geq E_{el,max}/n_{con,EL} + E_{comp,max,t}/n_{inv}$

Produced H₂ (in kg)

$$gm_{H2,t} = GM_{H2,t} \cdot \Delta t$$

Total mass of stored H₂ (in kg)

$$M_{H2,t} = M_{H2,t-1} + gm_{H2,t}$$

Residual energy $E_{res,t} = E_{pv,t} \cdot n_{con,pv} - (E_{load,t} + E_{comp,t})/n_{inv} - E_{el,max}/n_{con,EL}$

If $E_{res} \leq B_{nec} - E_{bat,t-1}$ then $E_{charge,t} = E_{res,t}$

If $E_{res} > B_{nec} - E_{bat,t-1}$ then $E_{charge,t} = B_{nec} - E_{bat,t-1}$
and $E_{waste,t} = E_{res,t} - (B_{nec} - E_{bat,t-1})$

Case A2.1.1.2 $E_{el,min}/n_{con,EL} + E_{comp,min,t}/n_{inv} < E_{S/D,t} < E_{el,max}/n_{con,EL} + E_{comp,max,t}/n_{inv}$

$$E_{el,t} = \left(E_{S/D,t} - \frac{E_{comp,t}}{n_{inv}} \right) \times n_{con,EL}$$

$$GM_{H2,t} = 0.0153 \times E_{el,t}^{0.95}$$

$$E_{comp,t} = 976.62 \times P_{cyl,t-1}^{0.27} \times GM_{H2,t}$$

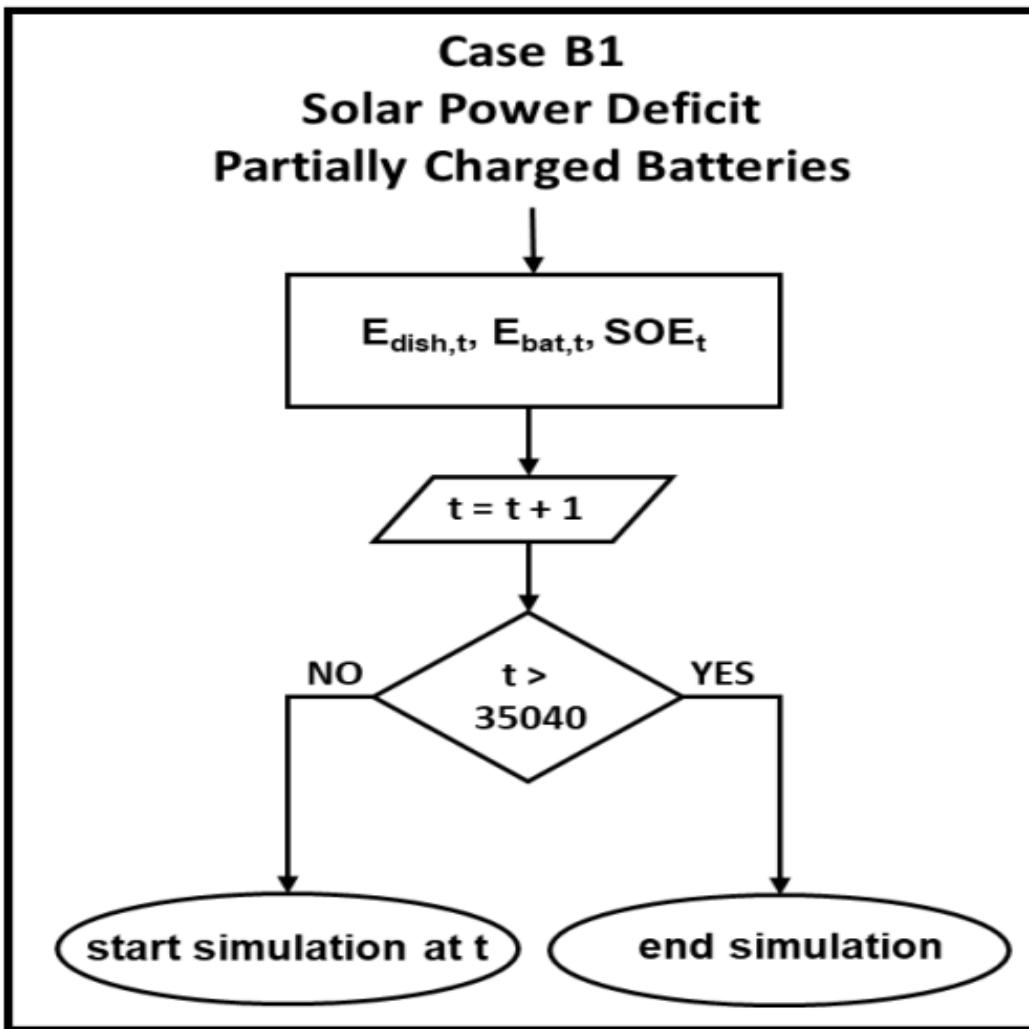
$E_{el,t}, GM_{H2,t}, E_{comp,t}$

Case A2.1.2 $E_{S/D,t} < E_{el,min}/n_{con,EL} + E_{comp,min,t}/n_{inv}$

$$E_{disch,t} = \frac{E_{el,min}}{n_{con,EL}} + \frac{E_{comp,min,t}}{n_{inv}} - E_{S/D,t}$$

Case B1: Solar energy deficit and partially discharged batteries.

$$E_{S/D,t} < 0 \text{ and } SOE_t > 20\%$$

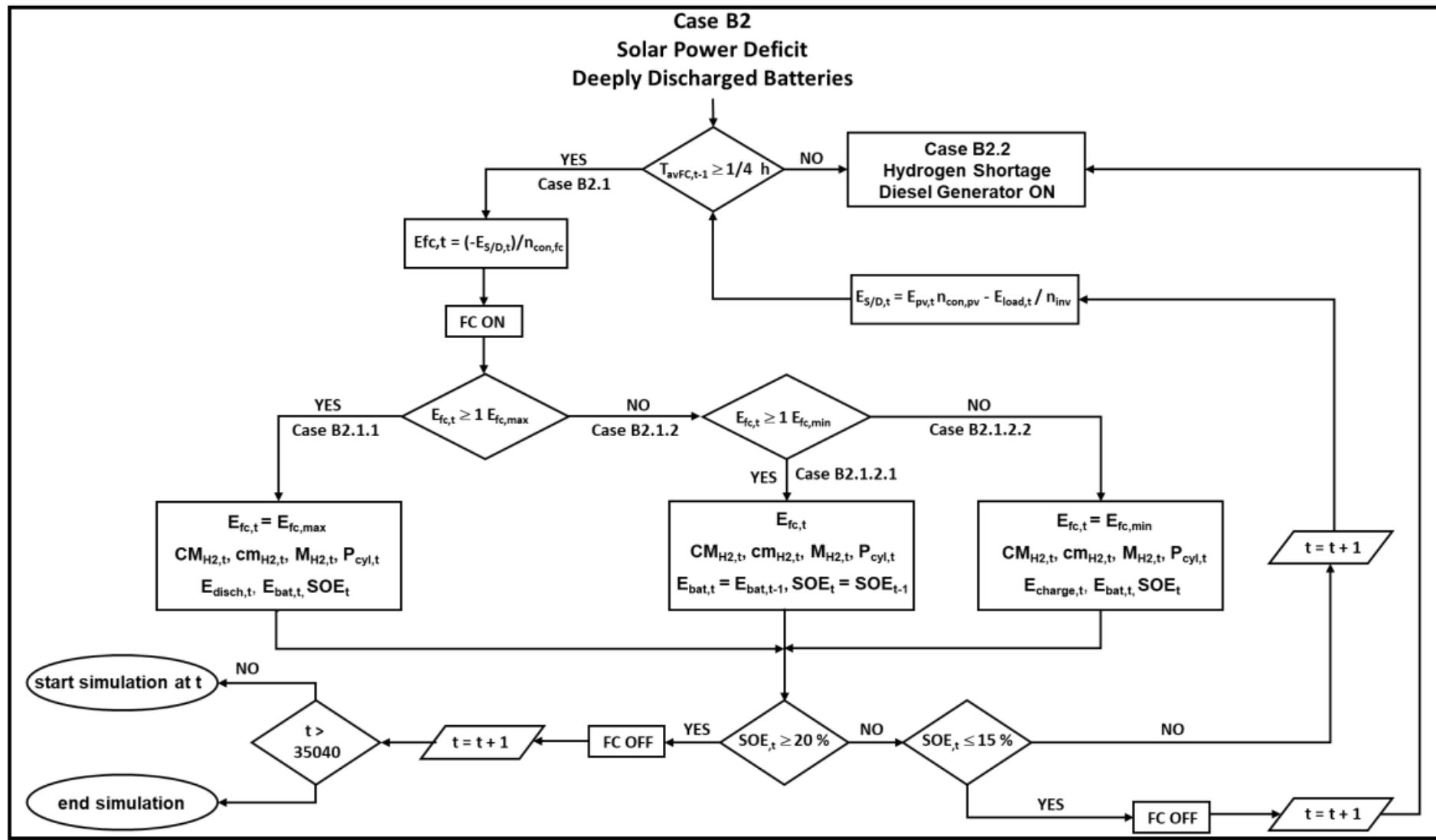


$$E_{disch,t} = \frac{E_{load,t}}{n_{inv}} - E_{PV,t} n_{con,pv}$$

$$E_{bat,t} = E_{bat,t-1} - E_{disch,t}$$

Case B2: Solar energy deficit and deeply discharged batteries.

$E_{S/D,t} < 0$ and $SOE < 20\%$



Case B2: Solar energy deficit and deeply discharged batteries.

Required time of FC to operate at its maximum power output

$$T_{avFC,t-1} = \frac{M_{H2,t-1} - M_{H2,min}}{CM_{H2,max}}$$

$M_{H2,t-1}$ and $M_{H2,min}$ are the stored H_2 mass (kg) at "t-1" and the defined minimum stored H_2 mass (kg), respectively.

*$CM_{H2,max}$ the maximum H_2 consumption, kg/hr $CM_{H2} = 2.78 * P_{FC}^2 + 33.17 * P_{FC} + 4.24$*

Case B2: Solar energy deficit and deeply discharged batteries.

Case B2.1: Fuel Cell operation (PV energy shortage, SOE \leq 20 % B_{NEC} , H₂ availability)

$$E_{fc,t} = \frac{-E_{S/D,t}}{n_{con,fc}} = \left(\frac{E_{load,t}}{n_{inv}} - E_{PV,t} \cdot n_{con,pv} \right) / n_{con,fc}$$

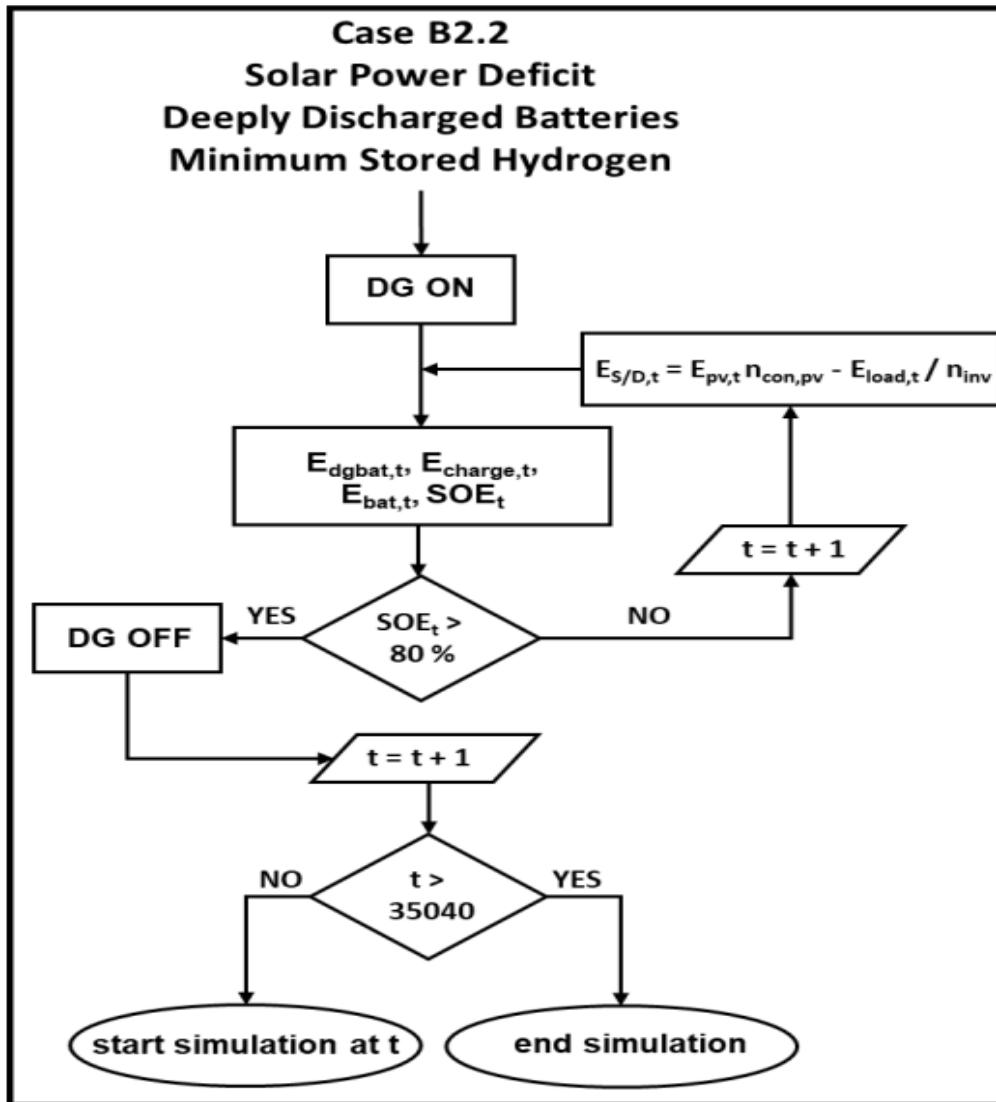
Case B2.1.1: For $E_{fc,t} > E_{fc,max}$  $E_{disch,t} = E_{fc,t} - E_{fc,max}$

Case B2.1.2: For $E_{fc,t} \leq E_{fc,max}$ 

Case B2.1.2.1, for $E_{fc,t} \geq E_{fc,min}$

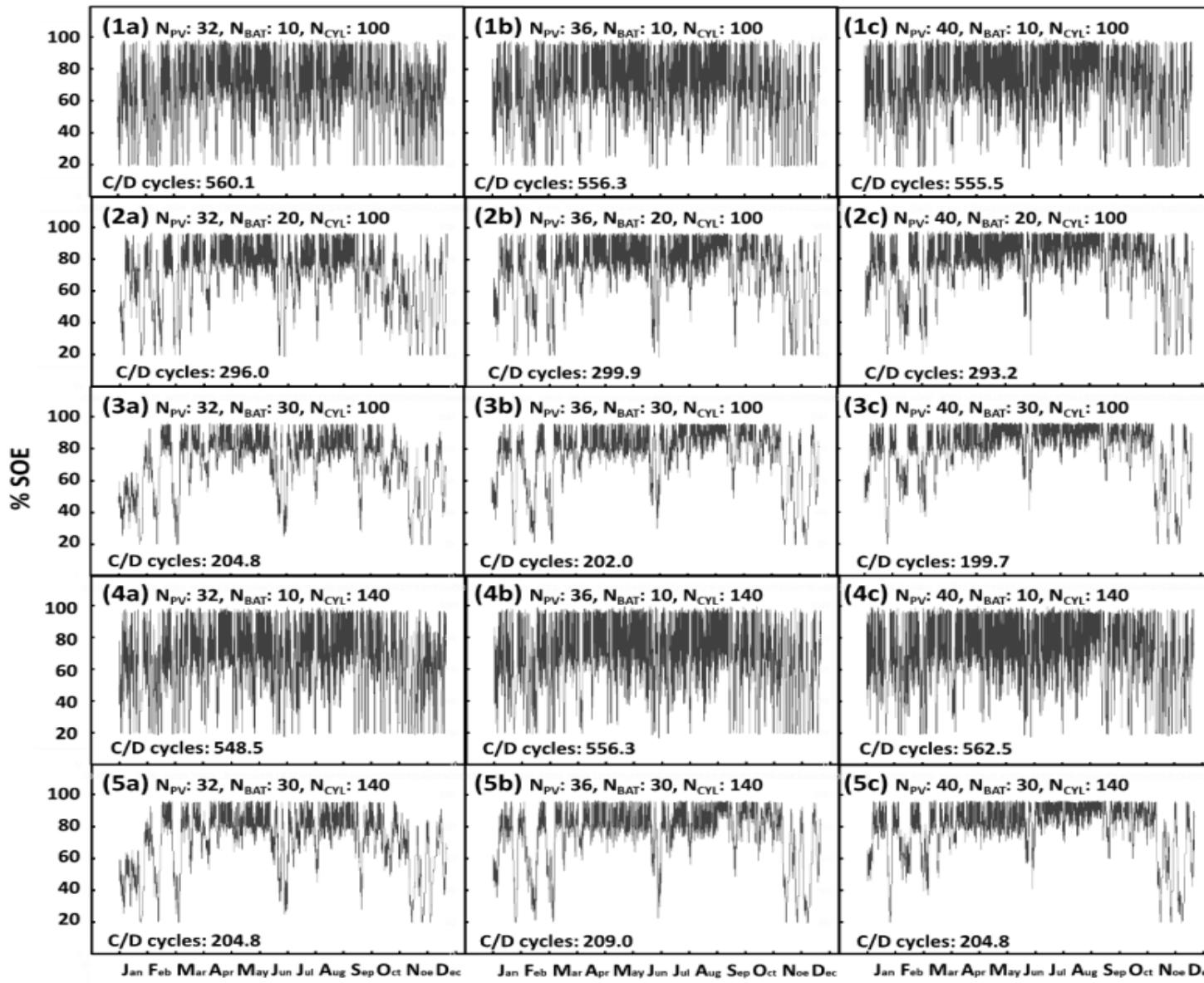
Case B2.1.2.2, for $E_{fc,t} < E_{fc,min}$  $E_{charge,t} = E_{fc,min} - E_{fc,t}$

Case B2.2, Operation of the Diesel Generator.



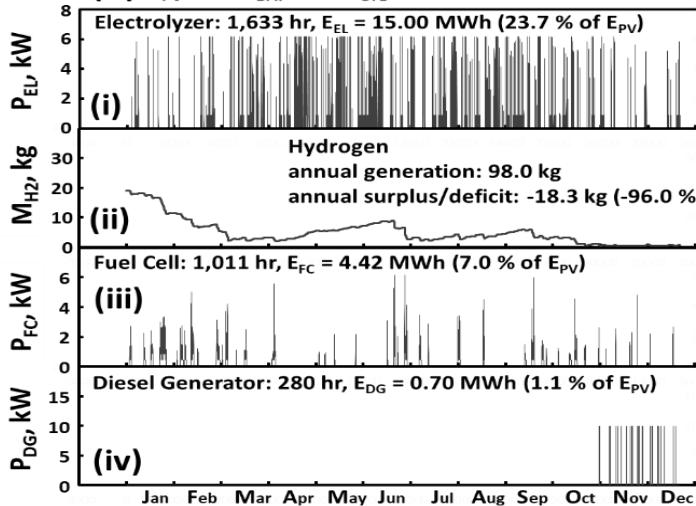
440 examined combinations of nominal PV power, battery's storage capacities and H₂ cylinders volumes (cylinder volumes 4 – 7 m³, corresponding to 80 – 140 cylinders).

*The batteries' bank state of energy (SOE) annual variation,
for selected $N_{PV}/N_{BAT}/V_{CYL}$ combinations.*

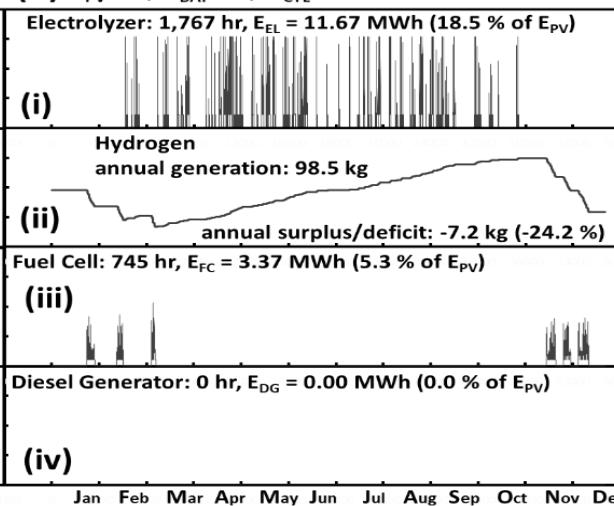


The hydrogen system and the diesel generator annual operation, for 5 m³ H₂ storage volume.

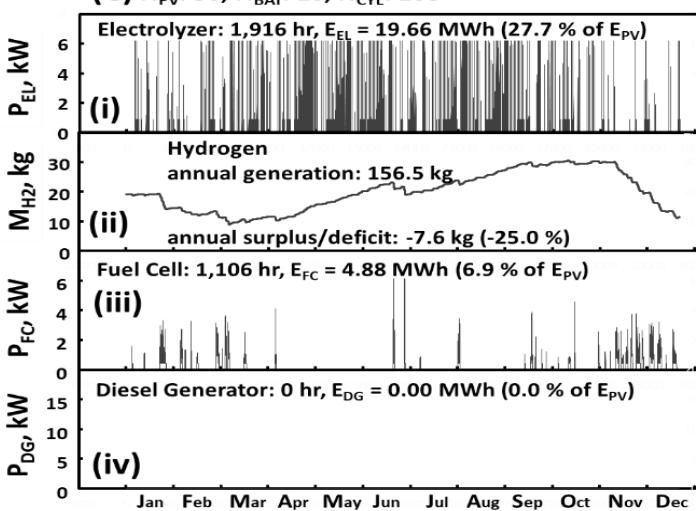
(A) N_{PV}: 32, N_{BAT}: 10, N_{CYL}: 100



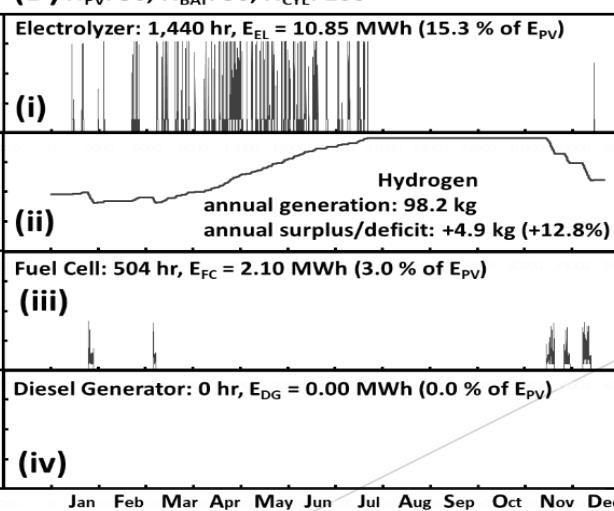
(B) N_{PV}: 32, N_{BAT}: 30, N_{CYL}: 100



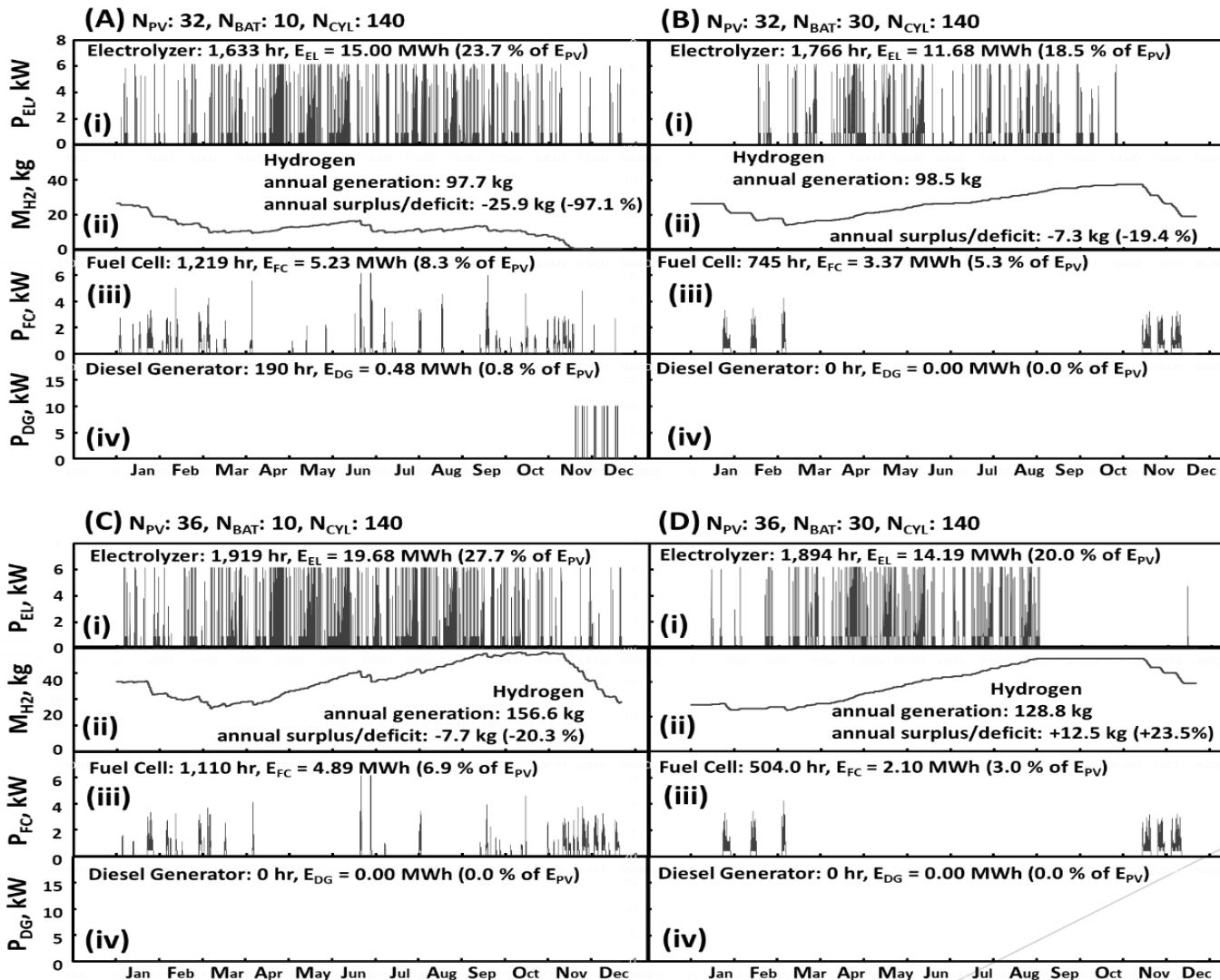
(C) N_{PV}: 36, N_{BAT}: 10, N_{CYL}: 100



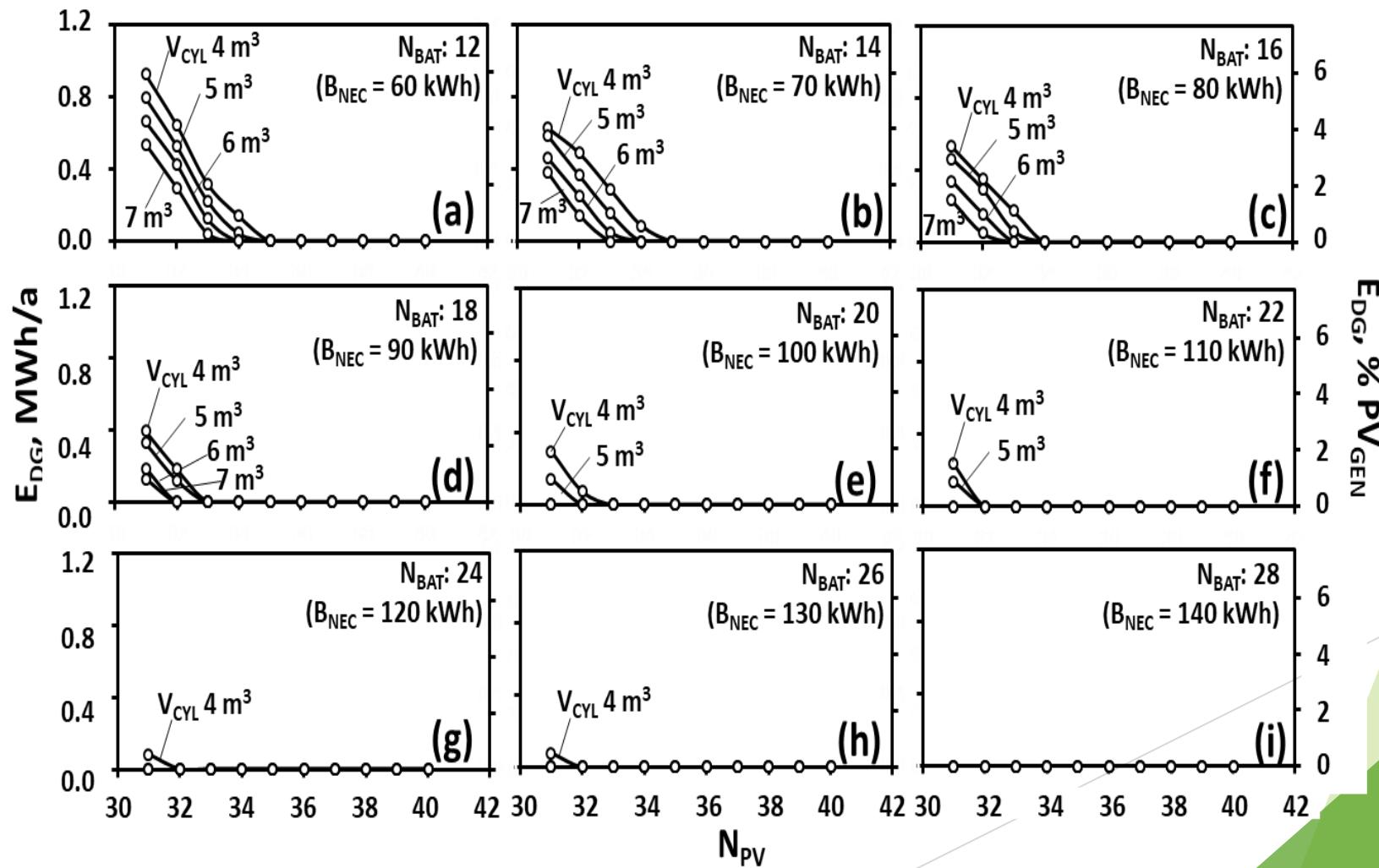
(D) N_{PV}: 36, N_{BAT}: 30, N_{CYL}: 100



The hydrogen system and the diesel generator annual operation, for 7 m³ H₂ storage volume.

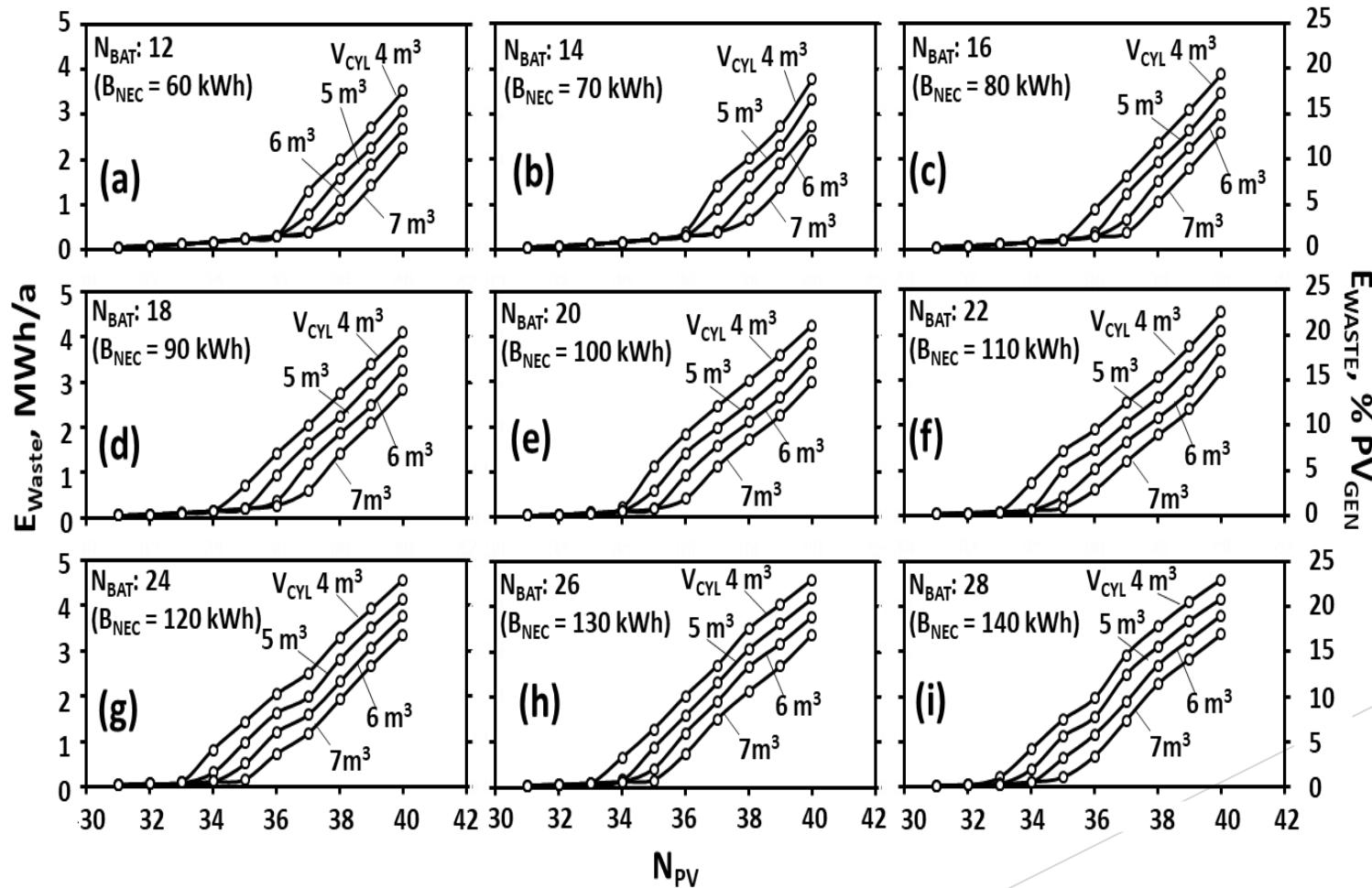


DG generation for B_{NEC} : 60 – 140 kWh, and the total examined number of PV modules and H_2 storage cylinders.



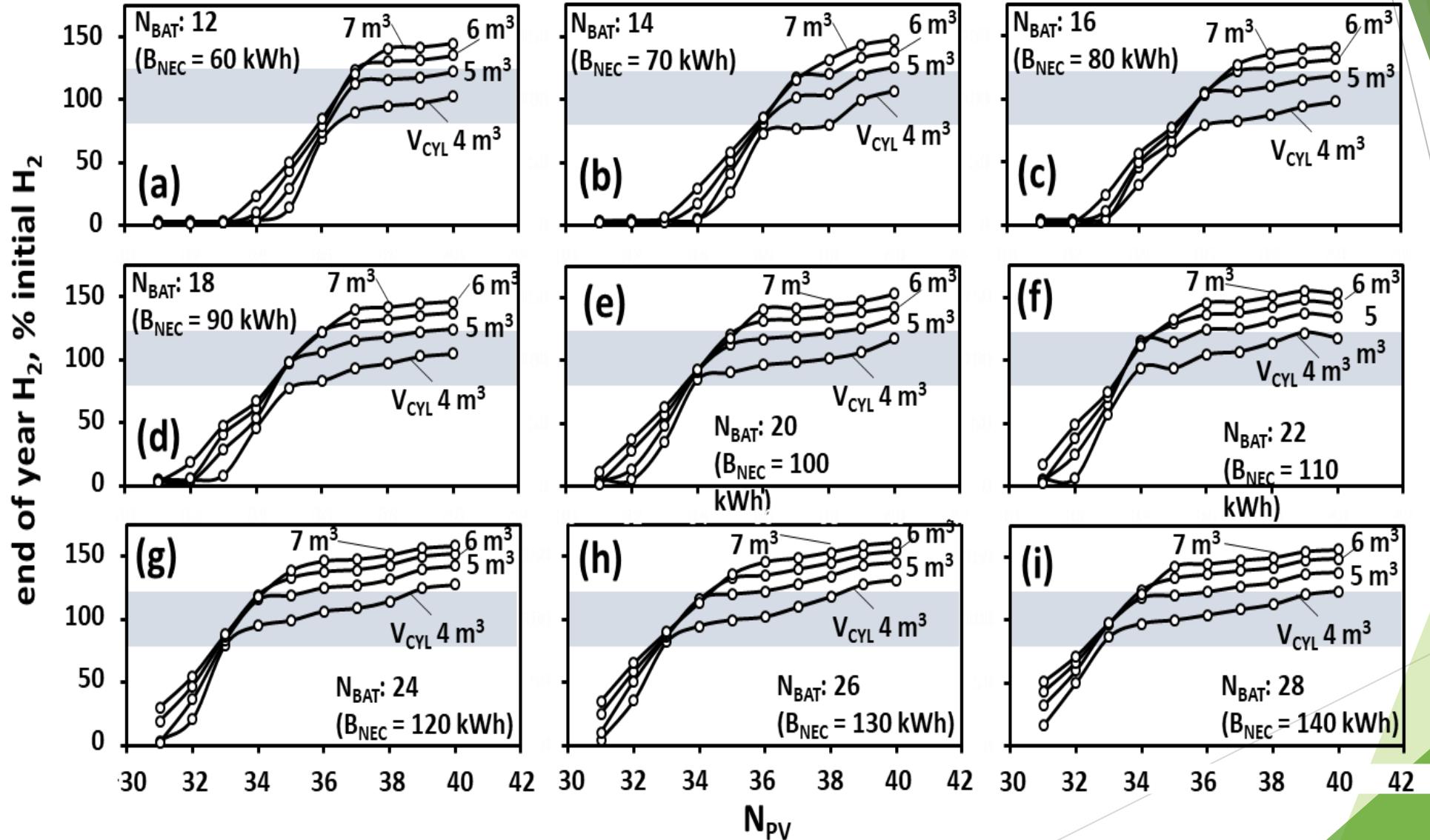
Required H₂ storage volumes (V_{CYL}, m₃) for zero DG generation, for the examined number of installed PV modules (N_{PV}) and batteries elements (N_{BAT}).

*Wasted PV generation for B_{NEC} : 60 – 140 kWh, and
the total examined number of PV modules and H_2 storage cylinders*



		N_{PV} – number of PV-modules in the PV-array (kW of the PV-array nominal power output)									
		31 (9.61)	32 (9.92)	33 (10.23)	34 (10.54)	35 (10.85)	36 (11.16)	37 (11.47)	38 (11.78)	39 (12.09)	40 (12.40)
N_{BAT} – number of battery elements in the battery bank (kWh of the battery bank capacity)	10 (50)	4-7	4-7	4-7	4-7	4-7	4-7	5-7	6-7		
	12 (60)	4-7	4-7	4-7	4-7	4-7	4-7	5-7			
	14 (70)	4-7	4-7	4-7	4-7	4-7	5-7	6-7			
	16 (80)	4-7	4-7	4-7	4-7	4-7	5-7	7			
	18 (90)	4-7	4-7	4-7	4-7	5-7	7				
	20 (100)	4-7	4-7	4-7	5-7	6-7					
	22 (110)	4-7	4-7	4-7	5-7	7					
	24 (120)	4-7	4-7	4-7	6-7	7					
	26 (130)	4-7	4-7	4-7	6-7	7					
	28 (140)	4-7	4-7	5-7	6-7						
	30 (150)	4-7	4-7	5-7	7						

*Hydrogen excesses or shortages, for BN_{EC}: 60 – 140 kWh,
and the total examined number of PV modules and H₂ storage cylinders*



Required H₂ storage volumes (V_{CYL}, m³) for the annual H₂ excesses/shortages within ± 20 % of initially stored H₂, for the examined N_{PV} and N_{BAT}.

		N _{PV} – number of PV-modules in the PV-array (kW of the PV-array nominal power output)									
		31 (9.61)	32 (9.92)	33 (10.23)	34 (10.54)	35 (10.85)	36 (11.16)	37 (11.47)	38 (11.78)	39 (12.09)	40 (12.40)
N _{BAT} – number of battery elements in the battery bank (kWh of the battery bank capacity)	10 (50)							4-7	4-5	4-5	4
	12 (60)						7	4-5	4-5	4-5	4
	14 (70)						5-7	5-7	4-5	4-5	4
	16 (80)					5-7	4-5	4-5	4-5	4-5	4-5
	18 (90)				5-7	4-5	4-5	4-5	4	4	4
	20 (100)			4-7	4-5	4-5	4-5	4	4	4	4
	22 (110)			4-7	4-5	4	4	4			
	24 (120)		4-7	4-7	4-5	4	4	4			
	26 (130)		4-7	4-7	4-5	4	4	4			
	28 (140)		4-7	4-5	4-5	4	4	4			
	30 (150)		4-7	4-5	4	4	4				

Required H₂ storage volumes (V_{CYL} m³) for:

- (i) zero DG generation,
 - (ii) zero waste and
 - (iii) annual H_2 excesses/shortages in the range of $\pm 20\%$ of initially stored H_2 ,

for the examined number of installed PV modules (N_{PV}) and batteries elements (N_{BAT}).